

## EXPERIMENTAL RESEARCH TO CHARACTERIZE POWDERS FROM REFRACTORY MATERIALS USED IN CASTING STEEL

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*In this paper, the authors present the properties and technology of obtaining some powdery refractory materials used in the steel casting process. The researches carried out to determine the most important physical and chemical properties of the refractory materials used as coating powders for steel casting are presented, namely viscosity and fusibility. The temperatures at which the eutectic occurs in the ternary systems  $\text{SiO}_2\text{-Al}_2\text{O}_3\text{-CaO}$  were determined. The influence of the  $\text{Al}_2\text{O}_3$  content in the raw materials on the viscosity of the casting powders at different temperatures was determined.*

**Keywords:** refractory materials, fusibility, slag viscosity, continuous casting, casting powders

### 1. Introduction

The use of ointments and heat-insulating materials has become a common practice in steelworks, their application leading to particularly important metal savings. The products included under this generic name represent lubricating powders, anti-retraction powders, masselot plates and powders for continuous casting.

Auxiliary materials used worldwide for steel casting are in a very diverse range both in the form of chemical compositions and in the form of raw materials used in their manufacture.

In current practice, lubrication and anti-seize materials are applied in the form of powders after packaging in polyethylene bags or in the form of shaped plates made of powders with a binder. [1-4]

From the documentation carried out, the imported casting powders are manufactured in several varieties depending on the place, the size of the ingot, the casting temperature, and the quality of the steel. [5-7].

Satisfaction of the casting powder functions is ensured by the chemical composition of the powder, which, by the proportion of oxides as well as by its other components, determines both the temperature and the melting-solidification

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range, falling within the ternary system  $\text{CaO-Al}_2\text{O}_3\text{-SiO}_2$  as well as in the  $\text{CaO-Al}_2\text{O}_3\text{-CaF}_2\text{-Na}_2\text{O}$ ,  $\text{CaO-Al}_2\text{O}_3\text{-SiO}_2\text{-CaF}_2\text{-Na}_2\text{O-C}$  systems.

## 2. Experimental

### 2.1. Chemical and mineralogical composition of casting powders

In this work was studied the possibility of producing a pilot batch of casting powders using the raw materials and the equipment of the research laboratory within the Center for Research, Design and Production - CCPPR SA Alba Iulia.

From a chemical point of view, casting powders are part of the metallurgical slag field, meaning the  $\text{SiO}_2\text{-CaO-Al}_2\text{O}_3$  system [1,2].

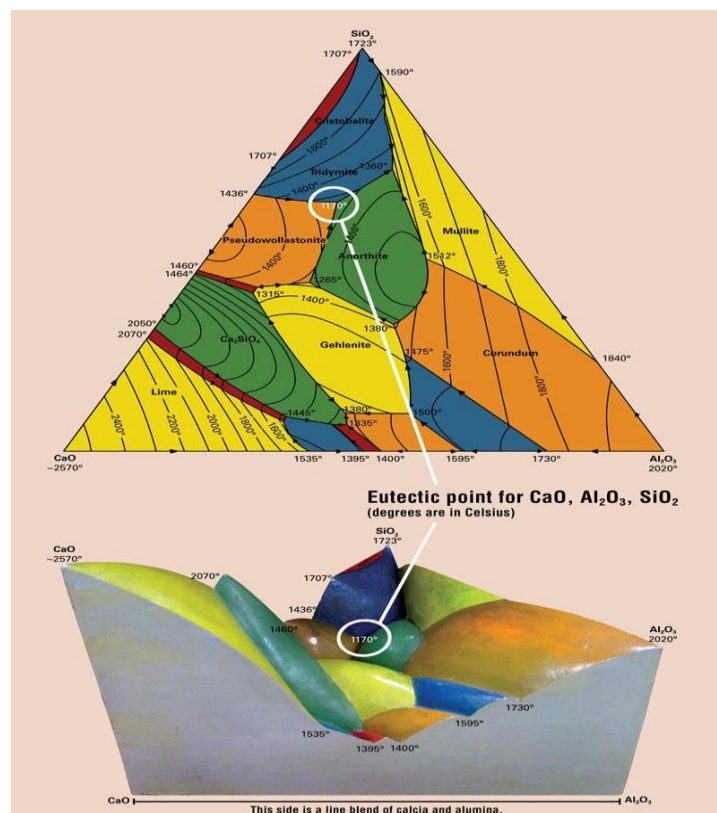


Fig. 1. Thermal balance diagram  $\text{SiO}_2\text{-CaO-Al}_2\text{O}_3$  [1]

The  $\text{SiO}_2\text{-CaO-Al}_2\text{O}_3$  system consists of:

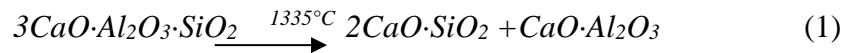
- ANORTIT ( $\text{Ca}$  felspat),  $\text{CaO} \cdot \text{Al}_2\text{O}_3 \cdot 2\text{SiO}_2$ : is congruent with melting point at  $1550^\circ\text{C}$ ; crystallizes into tricline blades; is a compound found in eruptive rocks and in technical silicates such as acid metallurgical slags.

- GHELENIT,  $2\text{CaO} \cdot \text{Al}_2\text{O}_3 \cdot \text{SiO}_2$ : is congruent with melting point  $1590^\circ\text{C}$ ; crystallizes into quartz crystalline forms.

-GRANAT,  $3\text{CaO} \cdot \text{Al}_2\text{O}_3 \cdot 3\text{SiO}_2$ ; is incongruent in the solid phase, therefore under normal pressure it does not appear in the presence of the liquid phase and does not appear in the equilibrium diagram of the system.

It does not appear in technical silicas but only in minerals that have formed at high pressures

-ALUMINOSILICATE TRICALCIUM  $3\text{CaO} \cdot \text{Al}_2\text{O}_3 \cdot \text{SiO}_2$ : is incongruent in solid form; crystallizes the rhombic and decomposes into the liquid phase, to balance.



## 2.2. Fusibility

Fusibility is the property that allows a casting powder to melt at a particular temperature or temperature range such that a liquid slag layer is formed on the free surface of the cast steel to provide a certain fluidity.

However, it is not enough to find an optimal melting temperature, but an optimal melting-solidification interval should also be achieved, which is based on the size of the surface of the steel bath.

Optimal melting range of the casting powders has been found to be within the range of  $1150\text{--}1300^\circ\text{C}$ .

In the  $\text{SiO}_2\text{--Al}_2\text{O}_3\text{--CaO}$  system there are three eutectics having melting temperatures in this range.

Table 1.

**Eutectic melting temperatures in the  $\text{SiO}_2\text{--Al}_2\text{O}_3\text{--CaO}$  system [1]**

Eutectic	$\text{SiO}_2$ %	$\text{CaO}$ %	$\text{Al}_2\text{O}_3$ %	Temperature $^\circ\text{C}$
E <sub>11</sub>	62	23,25	14,75	1165
E <sub>12</sub>	42	38	20	1265
E <sub>13</sub>	40	49	11	1310

It can be noticed, however, from the position of the points in the system that:

- E<sub>11</sub> can not be taken into study, being outside the optimal range,
- E<sub>12</sub> is at the limit of the range, with the  $\text{Al}_2\text{O}_3$  content being high,
- E<sub>13</sub> is at the upper limit of the temperature range.

For this reason, various fondants such as magnesium oxide, sodium oxide, fluorine, boron trioxide had to be tried.

## 2.3. Viscosity of casting powders.

According to the definition, viscosity is the force acting on the surface unit so as to maintain a velocity gradient  $\Delta v/dt$  between two layers inside the slag, and after Arrhenius the viscosity is a function of temperature:

$$\log \eta = \frac{E}{KT} + B$$

Where  $K=1$  when the tetrahedric structural groups are free.

In silicate melts the viscosity will decrease as the anions (structural groups) are less complex, so the more mobile they are.

For this reason a highly acidic slag with a structure  $(\text{SiO}_4)^-$  can not be used for steel casting. [6,7]

Several authors have found that the most suitable steel casting would be neutral or almost neutral, giving different values for the  $\text{CaO} / \text{SiO}_2$  ratio, most grouping in the range [2]:

$$\frac{\text{CaO}}{\text{SiO}_2} = 0,7 - 1,1$$

Practically, a direct relationship between viscosity and temperature could not be established.

Mixtures with higher melting temperatures and lower viscosity are known than other mixtures with lower melting temperatures.

Thus, it can be shown that in the  $\text{SiO}_2\text{-CaO-Al}_2\text{O}_3$  system, the more basic E13 mixtures have a lower viscosity than those in zone E11, more acidic, although the latter have lower melting temperatures of about  $100^\circ \text{C}$ . [8-11]

But as a general rule, raising the temperature leads to a decrease in viscosity.

#### **2.4. Experimental research to determine the influence of aluminum oxide content on casting powders and casting slag viscosity.**

It has been noted that the introduction of  $\text{Al}_2\text{O}_3$  into slags produces an increase in viscosity, being a "network trainer".

Not only the total amount of oxide influences the viscosity but also its ratio to the other oxides, such as  $\text{Al}_2\text{O}_3/\text{SiO}_2$ .

In order to establish a more precise correlation between temperature and  $\text{Al}_2\text{O}_3$  content in slags, we have worked out in the EXCEL and MATLAB calculation programs, the known data of casting powder compositions, especially the content of  $\text{Al}_2\text{O}_3$  of pubes and their properties.

These data processing allowed to establish dependencies between puberty  $\text{Al}_2\text{O}_3$  content and their properties, correlations represented both graphically and analytically in Figs. 2 - 13.

The multiple correlation allows the choice of optimal temperature and  $\text{Al}_2\text{O}_3$  values to determine viscosity in a certain range, Fig. 2.

Horizontally, subdomains of viscosity variation are shown.

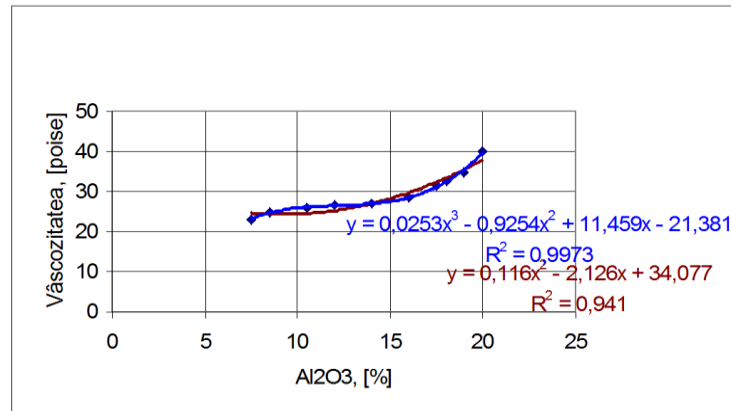


Fig. 2. The viscosity of the slag for continuous casting according to the content of Al<sub>2</sub>O<sub>3</sub> at a temperature of 1300° C [1]

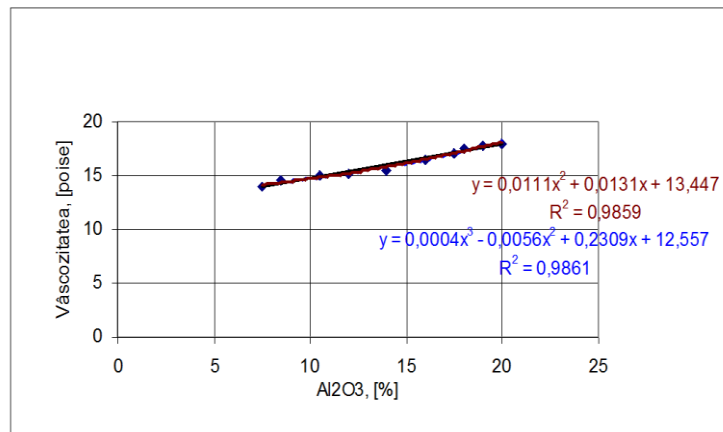


Fig. 3. The viscosity of the slag for continuous casting according to the content of Al<sub>2</sub>O<sub>3</sub> at a temperature of 1350° C [1]

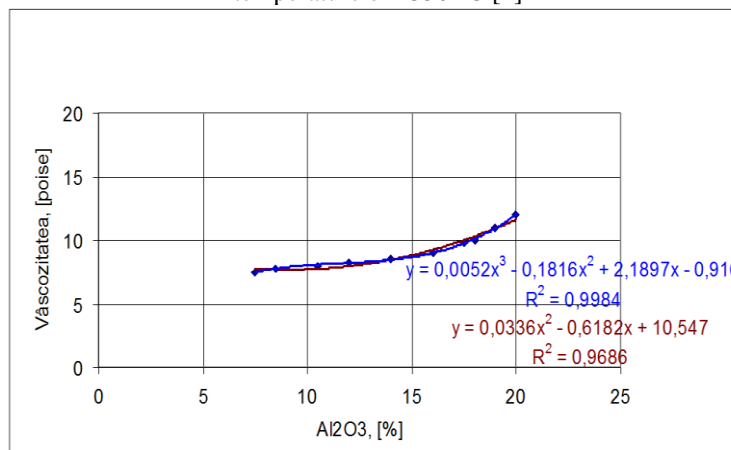


Fig. 4. The viscosity of the slag for continuous casting according to the content of Al<sub>2</sub>O<sub>3</sub> at a temperature of 1400° C [1]

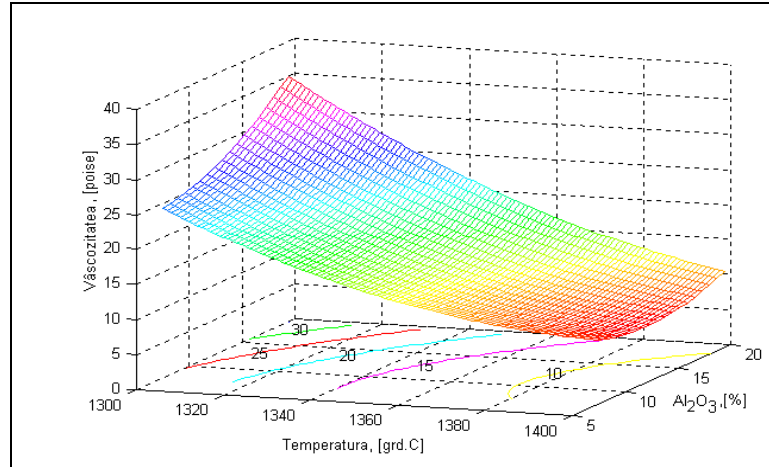


Fig. 5. The viscosity of the slag for continuous casting according to the temperature and the content of  $\text{Al}_2\text{O}_3$  [1]

From the practical data it was found that the viscosity is influenced not only by the total amount of  $\text{Al}_2\text{O}_3$  introduced but also by its ratio to the other oxides, the most representative being the ratio of  $\text{Al}_2\text{O}_3 / \text{SiO}_2$ .

These dependencies are obtained by processing the data in the MATLAB program.

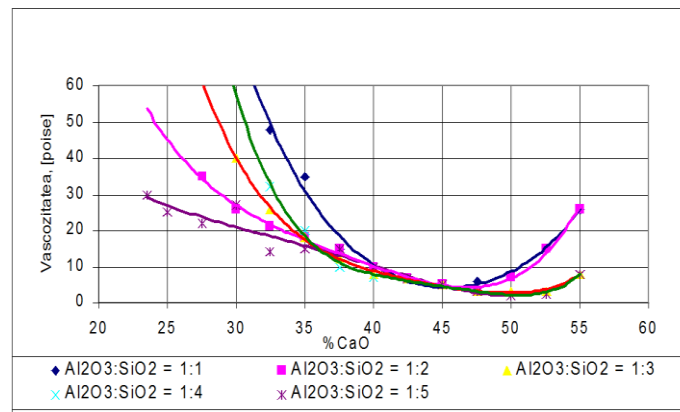


Fig. 6. Influence of  $\text{Al}_2\text{O}_3 / \text{SiO}_2$  ratio on viscosity for 0% MgO [1]

In order to obtain an expressed and analytical dependence between viscosity and the CaO content of slag, 0% MgO and different values of the  $\text{Al}_2\text{O}_3 / \text{SiO}_2$  ratio, we present the results obtained in the Figs.. 13 also present the same variation but at different MgO contents, as follows: for 5% MgO, 10% MgO and 15% MgO.

It can be noticed that with the increase of the percentage of MgO in the slag composition, there is a decrease of the viscosity values, falling within increasingly narrow limits.

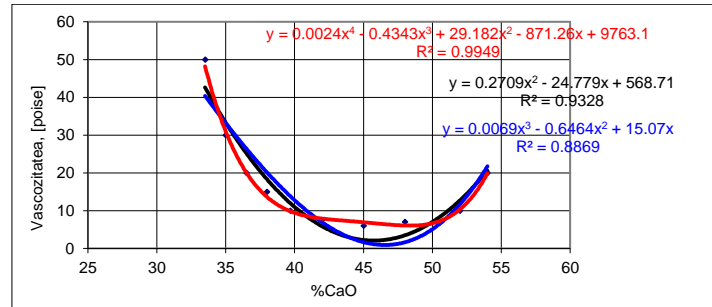


Fig. 7. Influence of  $\text{Al}_2\text{O}_3/\text{SiO}_2$  ratio=1/1 on viscosity for 0% MgO [1]

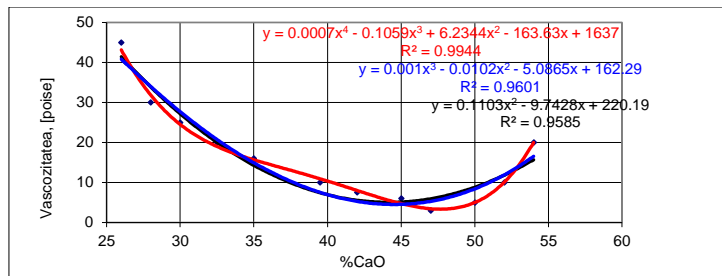


Fig. 8. Influence of  $\text{Al}_2\text{O}_3/\text{SiO}_2$  ratio=1/2 on viscosity for 0% MgO [1]

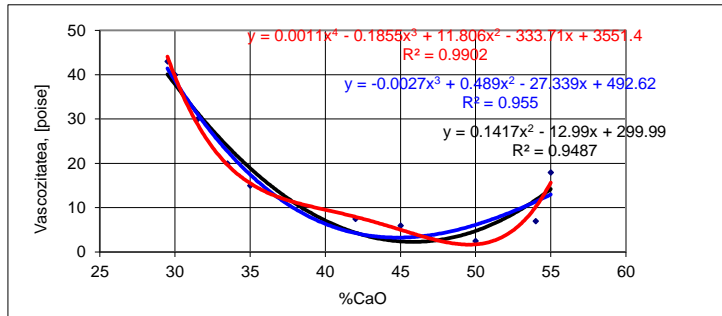


Fig. 9. Influence of  $\text{Al}_2\text{O}_3/\text{SiO}_2$  ratio=1/3 on viscosity for 0% MgO [1]

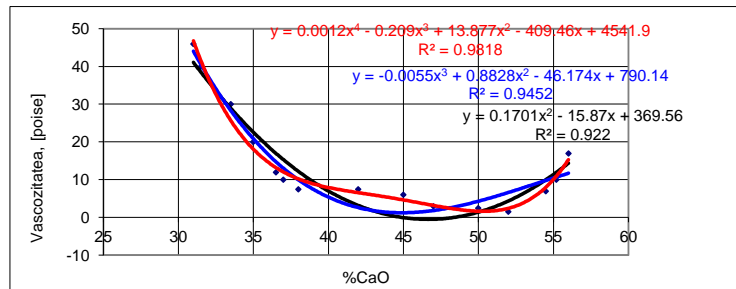
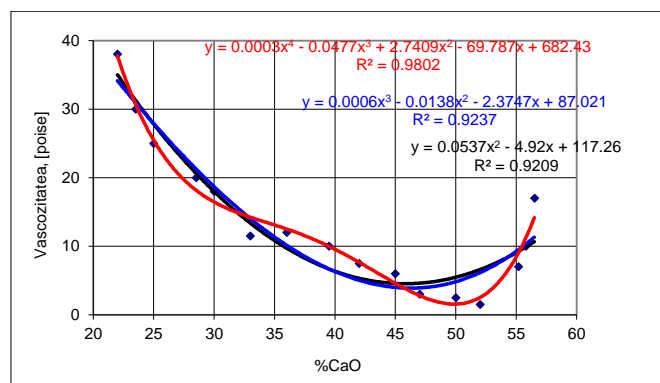
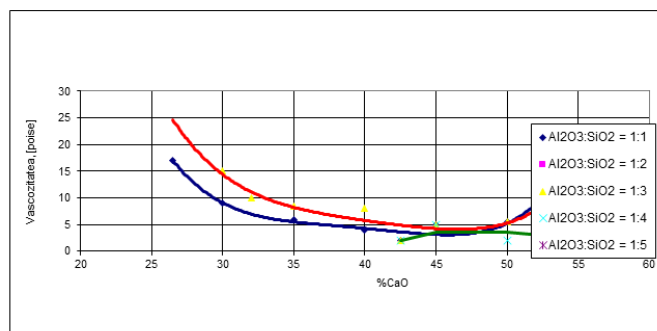
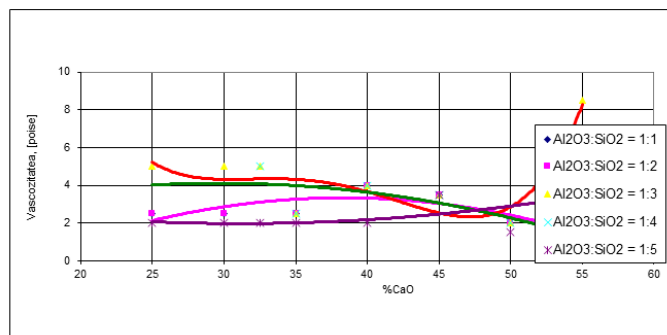


Fig. 10. Influence of  $\text{Al}_2\text{O}_3/\text{SiO}_2$  ratio=1/4 on viscosity for 0% MgO [1]

Fig. 11. Influence of  $\text{Al}_2\text{O}_3/\text{SiO}_2$  ratio=1/5 on viscosity for 0% MgO [1]Fig. 12. Influence of the  $\text{Al}_2\text{O}_3/\text{SiO}_2$  ratio on viscosity at 5% MgO [1]Fig. 13. Influence of  $\text{Al}_2\text{O}_3/\text{SiO}_2$  ratio on viscosity at 15% MgO [1]

### 3. Results and discussions

From the qualitative characteristics determined in the laboratory conditions, the data presented in Table 1 and Figs. 2-13 reveals the following aspects:

-In Figs. 2, 3 and 4 show that the viscosity increases with the increase in  $\text{Al}_2\text{O}_3$  content, the best statistical correlation being the 3rd degree polynomial equation, with  $R=0.9984$ .



-In Fig. 6 shows that viscosity decreases with increasing temperature but increases with increasing  $\text{Al}_2\text{O}_3$  content

-In Figs. 7 and 8, it can be seen that the viscosity decreases with the increase in the percentage of CaO, the minimum viscosity value being recorded at approximately 45% CaO, after which it slightly increases.

The best correlation between viscosity and CaO content is represented by the 4th degree polynomial, where the correlation coefficient is 0.9944.

-In Figs. 9, 10 and 11 it can be seen that the decrease in the viscosity value with the CaO content is more pronounced with the decrease in the ratio between  $\text{SiO}_2$  and  $\text{Al}_2\text{O}_3$ .

-In Figs. 12 and 13 show the influence of magnesium oxide content, which lowers viscosity values depending on CaO.

#### 4. Conclusions

Casting powders, in their various forms of lubrication, coating and continuous casting, are of particular importance in the steel casting process.

The research carried out in the present work showed that the quality and possibilities of use of a refractory product cannot be determined by knowing only one or two of its properties, but all of its chemical and physicochemical properties, which are closely dependent, must be taken into account.

The initial content of  $\text{Al}_2\text{O}_3$  in slag is not decisive for casting slag, it becomes saturated around 30%  $\text{Al}_2\text{O}_3$ , but the continuous flow of the slag powder as usual does not reach this value.

The increase in viscosity at the introduction of  $\text{Al}_2\text{O}_3$  is due to the fact that this oxide forms octahedral  $(\text{AlO}_6)^{9-}$  instead of tetrahedra  $(\text{AlO}_4)^{5-}$ , bonding the free ends of the silicate chains or those having the last  $\text{Ca}^{2+}$  bonded oxygen.

For the most rational choice of the casting powder, the specific operating conditions must be known, as well as its most important properties.

The satisfaction of the functions of the casting powders is ensured by the chemical composition of the powder, which, through the proportion of oxides, as well as through its other components, determines both the temperature and the melting-solidification interval, falling within the  $\text{CaO}-\text{Al}_2\text{O}_3-\text{SiO}_2$  ternary system.

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