

MATRIX MODEL IN INVERSE DYNAMICS OF A 3-DOF SPATIAL PARALLEL MANIPULATOR

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În timp ce cinematica roboților a fost studiată în bună măsură în ultimele două decenii, puține lucrări de dinamica roboților paraleli pot fi identificate. Lucrarea prezintă stabilște unele relații matriceale recursive pentru cinematica și dinamica unui manipulator paralel spațial cu trei grade de libertate: două translații și o rotație. Presupunând că poziția și mișcarea platformei mobile este cunoscută și utilizând o nouă metodă matriceală, se prezintă o formulare dinamică inversă. În ultima parte a lucrării sunt determinate câteva relații matriceale iterative și grafice pentru forțele celor trei sisteme de acționare.

While the robot kinematics has been studied extensively during the last two decades, fewer papers can be found on the dynamics of parallel robots. Some recursive matrix relations for the kinematics and dynamics of a spatial parallel manipulator, which has two translational degrees of freedom and one rotational degree of freedom, are established in this paper. Supposing that the position and the motion of the mobile platform are known and using a new matrix method, an inverse dynamic formulation is presented. Finally, some iterative matrix relations and some graphs for forces of the three actuators are determined.

Keywords: dynamics, manipulator, matrix, platform, simulation

Introduction

Parallel manipulators are closed-loop mechanisms presenting very good performances in terms of accuracy, rigidity and stability to manipulate large loads. These mechanisms generally compose two platforms, which are connected by joints and legs acting in parallel. One of them is attached to the fixed reference base. The other one can have arbitrary motion in its workspace. Several mobile legs or limbs, made up as serial robots, connect a movable platform to the fixed frame. Typically, the number of actuators is equal to the number of degrees of freedom. Compared with commonly known serial robots, parallel manipulators have some special characteristics: greater structural rigidity, potentially higher precision, stable functioning, larger capacity and suitable position of the actuating systems. There has been great amount of research on the application of parallel

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manipulators, such as machine tools [23] and industrial robots [2]. When good dynamic performance and precise positioning under high load are required, the dynamic model is important for their control.

In the last few years the parallel manipulators with less DOF have attracted the researchers and some of them have been used in the structure design of robotic manipulators. Parallel mechanisms can be found in many technical applications in which it is desired to orient a rigid body in space of high speed. Accuracy and precision in the execution of the task are essential since the robot is intended to operate on fragile objects; any errors in the positioning of the tool could lead to expensive damage. Recently, many efforts have been devoted to the kinematics and dynamic analysis of fully parallel manipulators. Many companies have developed them as high precision machine tools. The most known application is the aircraft simulator with six degrees of freedom, which is in fact the Stewart-Gough platform. A lot of works have focused on the dynamics of this parallel manipulator ([4], [8], [14], [22], [26], [27]). Geng [6] developed Lagrange's equations of motion under some simplifying assumptions regarding the geometry and inertia distribution of the manipulator. Dasgupta and Mruthyunjaya [4] used the Newton-Euler approach to develop closed-form dynamic equations of Stewart platform, considering all dynamic and gravity effects as well as viscous friction at joints. They observed that the application of the Newton-Euler method is more economical in the case of parallel or hybrid manipulators than in serial robots. Pierrot and Company [15] presented a new family of parallel robots with 4-DOF. The parallel manipulator Star [7] and the parallel Delta robot ([1], [21], [24], [25], [30]) equipped with three engines, which have a parallel setting, train on the effector in a three degrees of freedom general translation motion.

In this paper, a new matrix approach is adopted to derive the inverse dynamic equations of a spatial parallel manipulator [10], which has two translation degrees of freedom and one rotational degree of freedom (Fig. 1).

1. Geometric model of the manipulator

The spatial mechanism consists of three kinematical closed chains, including three variable length limbs. The motion of the platform is accomplished by the slide of three sliders of mass m_1 on the guide-ways.

The moving platform is an isosceles triangle $A_3B_3C_5$, which is described by the sizes $A_3B_3 = 2r$, $A_3C_5 = B_3C_5 = r\sqrt{2}$. It has the mass m_3 and the tensor of inertia \hat{J}_3 (Fig. 2). This platform is connected to a fixed platform, which consists of a three guide-ways (2), (7) and (9), through the legs (1), (8) and (12). Parameter R denotes the size of the base platform, where $A_2B_2 = 2R$, $A_2C_2 = B_2C_2 = R$. The legs (1) and (12), have identical chains, consisting of a constant link which is

connected to a universal joint at the bottom end and a passive revolute joint at the other. These legs have also the length L , the same mass m_2 and the same tensor of inertia \hat{J}_2 . The revolute joint is then attached to an active slider, which is mounted on the guide-way (2) or (9). The third leg (8) consists of an active prismatic system, a revolute joint that is attached to a third slider, an intermediary mechanism with four revolute joints that connect a planar four-bar parallelogram. This classical mechanism is finally connected to the moving platform.

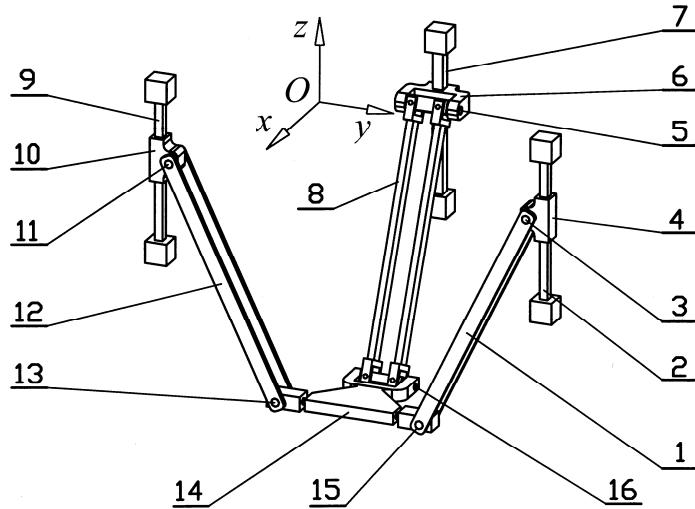


Fig. 1 Spatial parallel manipulator

Let $Ox_0y_0z_0(T_0)$ be a global frame, located at the centre of the side A_2B_2 with the Oz_0 axis normal to the base platform and the Oy_0 axis along A_2B_2 . The three-degrees-of-freedom manipulator is moving with respect to this Cartesian referential. One of three active elements of the robot is the first body C_1 of the limb C , for example. This slider is mounted on the guide way (7) and effect a vertical translation with the displacement λ_{10}^C . A local leg frame $C_2x_2^C y_2^C z_2^C$ is attached to a horizontal transmission bar with its origin at point C_2 , the $C_2z_2^C$ direction along the horizontal rotating axis of the revolute joint. This bar has a relative rotation with the angle φ_{21}^C . Further on, two identical bars with length L , same mass m_2 and same tensor of inertia \hat{J}_2 , rotates about the T_2^C frame with the angle $\varphi_{32}^C = \varphi_{62}^C$. The parallelogram of the leg C is closed by an element T_4^C , which has the same dimensions with T_2^C .

The displacements $\lambda_{10}^A, \lambda_{10}^B, \lambda_{10}^C$ of the three actuators A_1, B_1, C_1 are considered as parameters, which give the position of the mechanism. But, in the inverse geometric problem, one can suppose that the coordinates y_0^P, z_0^P of the point P and the rotational angle θ of the platform, give the position of the mechanism.

Pursuing the legs A, B, C , one obtains the following passing matrices

$$\begin{aligned} a_{10} &= a_1, a_{21} = a_{21}^\varphi a_\alpha a_4 \\ b_{10} &= a_2, b_{21} = b_{21}^\varphi a_\alpha a_4 \\ c_{10} &= a_3, c_{21} = c_{21}^\varphi a_\alpha a_4 \\ c_{32} &= c_{32}^\varphi a_4, c_{43} = c_{32}^\varphi a_5 \\ c_{54} &= c_{54}^\varphi a_\alpha a_6, c_{62} = c_{32}^\varphi a_4, \end{aligned} \quad (1)$$

where one denoted ([17])

$$\begin{aligned} a_1 &= \begin{bmatrix} 0 & -1 & 0 \\ 1 & 0 & 0 \\ 0 & 0 & 1 \end{bmatrix}, a_2 = \begin{bmatrix} 0 & 1 & 0 \\ -1 & 0 & 0 \\ 0 & 0 & 1 \end{bmatrix}, a_3 = \begin{bmatrix} -1 & 0 & 0 \\ 0 & -1 & 0 \\ 0 & 0 & 1 \end{bmatrix} \\ a_4 &= \begin{bmatrix} 0 & 0 & -1 \\ -1 & 0 & 0 \\ 0 & 1 & 0 \end{bmatrix}, a_5 = \begin{bmatrix} -1 & 0 & 0 \\ 0 & 1 & 0 \\ 0 & 0 & -1 \end{bmatrix}, a_6 = \begin{bmatrix} 0 & 0 & -1 \\ 0 & -1 & 0 \\ -1 & 0 & 0 \end{bmatrix} \\ a_\alpha &= \begin{bmatrix} \cos \alpha & \sin \alpha & 0 \\ -\sin \alpha & \cos \alpha & 0 \\ 0 & 0 & 1 \end{bmatrix}, a_{k,k-1}^\varphi = \begin{bmatrix} \cos \varphi_{k,k-1}^A & \sin \varphi_{k,k-1}^A & 0 \\ -\sin \varphi_{k,k-1}^A & \cos \varphi_{k,k-1}^A & 0 \\ 0 & 0 & 1 \end{bmatrix} \\ a_{k0} &= \prod_{j=1}^k a_{k-j+1,k-j} \end{aligned} \quad (2)$$

Rotation condition of the platform is given by the following identity

$$c_{50}^{\circ T} c_{50} = a \quad (3)$$

and by the matrices

$$c_{50}^{\circ} = \begin{bmatrix} 1 & 0 & 0 \\ 0 & 0 & -1 \\ 0 & 1 & 0 \end{bmatrix}, a = R^T = \begin{bmatrix} \cos \theta & 0 & -\sin \theta \\ 0 & 1 & 0 \\ \sin \theta & 0 & \cos \theta \end{bmatrix}, \quad (4)$$

where a is the rotation matrix around Py_A axis. From this relation, one obtains $\theta = \varphi_{54}^C - \varphi_{21}^C$.

Considering that the platform moves for one second and the motion's trajectory of the movable platform is given as

$$\begin{aligned}\vec{r}_0^P &= [0 \quad y_0^P \quad z_0^P - h]^T \\ y_0^P &= -t^2(t^2 - 1.3t + 0.3) \\ z_0^P &= 0.2t^2(2t^2 - t - 1) \\ \theta &= 0.4\sin(4\pi t),\end{aligned}\tag{5}$$

the displacements $\lambda_{10}^A, \lambda_{10}^B, \lambda_{10}^C$ and the angles $\varphi_{21}^A, \varphi_{21}^B, \varphi_{21}^C, \varphi_{32}^C$ are given by the following geometric constraint conditions

$$\begin{aligned}\vec{r}_{10}^A + a_{20}^T \vec{r}_{32}^A - a^T \vec{r}_{A_3} &= \vec{r}_0^P \\ \vec{r}_{10}^B + b_{20}^T \vec{r}_{32}^B - b^T \vec{r}_{B_3} &= \vec{r}_0^P \\ \vec{r}_{10}^C + c_{20}^T \vec{r}_{43}^C + c_{50}^T \vec{r}_5^P &= \vec{r}_0^P,\end{aligned}\tag{6}$$

where one denoted :

$$\begin{aligned}\vec{u}_1 &= \begin{bmatrix} 1 \\ 0 \\ 0 \end{bmatrix}, \vec{u}_2 = \begin{bmatrix} 0 \\ 1 \\ 0 \end{bmatrix}, \vec{u}_3 = \begin{bmatrix} 0 \\ 0 \\ 1 \end{bmatrix}, \tilde{\vec{u}}_3 = \begin{bmatrix} 0 & -1 & 0 \\ 1 & 0 & 0 \\ 0 & 0 & 0 \end{bmatrix} \\ \vec{r}_{10}^A &= \begin{bmatrix} 0 \\ -R \\ \lambda_{10}^A \end{bmatrix}, \vec{r}_{10}^B = \begin{bmatrix} 0 \\ R \\ \lambda_{10}^B \end{bmatrix}, \vec{r}_{10}^C = \begin{bmatrix} -R \\ 0 \\ \lambda_{10}^C \end{bmatrix} \\ \vec{r}_{32}^A &= L\vec{u}_1, \vec{r}_{32}^B = L\vec{u}_1, \vec{r}_{43}^C = -L\vec{u}_2 \\ \vec{r}_{A_3} &= -r\vec{u}_2, \vec{r}_{B_3} = r\vec{u}_2, \vec{r}_5^P = r\vec{u}_1 \\ h &= \sqrt{L^2 - (R - r)^2}, \sin \alpha = \frac{R - r}{L}, \cos \alpha = \frac{h}{L} \\ z_1 &= \lambda_{10}^A + h, z_2 = \lambda_{10}^B + h, z_3 = \lambda_{10}^C + h.\end{aligned}\tag{7}$$

2. Inverse kinematics analysis

The geometry and the motion capability of spatial manipulator has been analysed by Liu [11]. For inverse kinematics, the velocities and accelerations formulae are derived now in matrix closed form. Because the leg (1) and (2) have one rotational degree of freedom about the $A_2z_2^A$ and $B_2z_2^B$ axis, the angular velocities and angular accelerations can be written

$$\vec{\omega}_{20}^A = \dot{\varphi}_{21}^A \vec{u}_3, \vec{\omega}_{20}^B = \dot{\varphi}_{21}^B \vec{u}_3, \vec{\varepsilon}_{20}^A = \ddot{\varphi}_{21}^A \vec{u}_3, \vec{\varepsilon}_{20}^B = \ddot{\varphi}_{21}^B \vec{u}_3.\tag{8}$$

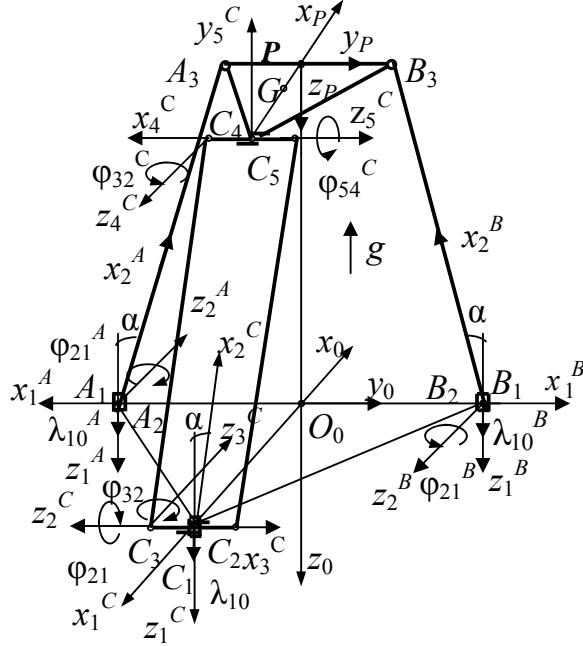


Fig. 2 Kinematical scheme of the mechanism

Velocities and accelerations of sliders A_1, B_1 and joints A_2, B_2 can be obtained as

$$\begin{aligned}\vec{v}_{10}^A &= \dot{\lambda}_{10}^A \vec{u}_3, \vec{v}_{10}^B = \dot{\lambda}_{10}^B \vec{u}_3, \vec{v}_{20}^A = a_{21} \vec{v}_{10}^A, \vec{v}_{20}^B = b_{21} \vec{v}_{10}^B \\ \vec{\gamma}_{10}^A &= \ddot{\lambda}_{10}^A \vec{u}_3, \vec{\gamma}_{10}^B = \ddot{\lambda}_{10}^B \vec{u}_3, \vec{\gamma}_{20}^A = a_{21} \vec{\gamma}_{10}^A, \vec{\gamma}_{20}^B = b_{21} \vec{\gamma}_{10}^B.\end{aligned}\quad (9)$$

On the other hand, leg (8) has two rotational degrees of freedom. The kinematics of components of chain $C_2 C_3 C_4 C_5$ are characterised by the matrices ([18]):

$$\vec{\omega}_{k0}^C = c_{k,k-1} \vec{\omega}_{k-1,0}^C c_{k,k-1}^T + \omega_{k,k-1}^C \vec{u}_3, \quad (10)$$

which are *associated* to absolute angular velocities given by recurrence relations

$$\vec{\omega}_{k0}^C = c_{k,k-1} \vec{\omega}_{k-1,0}^C + \omega_{k,k-1}^C \vec{u}_3, \omega_{k,k-1}^C = \dot{\phi}_{k,k-1}^C. \quad (11)$$

Following relation give the absolute velocity \vec{v}_{k0}^C of joint C_k :

$$\vec{v}_{k0}^C = c_{k,k-1} \{ \vec{v}_{k-1,0}^C + \vec{\omega}_{k-1,0}^C \vec{r}_{k,k-1}^C \}, \vec{v}_{10}^C = \dot{\lambda}_{10}^C \vec{u}_3, (k = 2, 3, 4, 5) \quad (12)$$

Absolute angular accelerations $\vec{\epsilon}_{k0}^C$ and accelerations $\vec{\gamma}_{k0}^C$ of joint C_k can be deduced from the time derivative of equations (10), (11), (12):

$$\begin{aligned}
\vec{\varepsilon}_{k0}^C &= c_{k,k-1} \vec{\varepsilon}_{k,k-1}^C + \varepsilon_{k,k-1}^C \vec{u}_3 + \omega_{k,k-1}^C c_{k,k-1} \tilde{\omega}_{k-1,0}^C c_{k,k-1}^T \vec{u}_3, \quad \varepsilon_{k,k-1}^C = \ddot{\varphi}_{k,k-1}^C \\
\tilde{\omega}_{k0}^C \tilde{\omega}_{k0}^C + \tilde{\varepsilon}_{k0}^C &= \omega_{k,k-1}^C \omega_{k,k-1}^C \tilde{u}_3 \tilde{u}_3 + \varepsilon_{k,k-1}^C \tilde{u}_3 \\
&+ c_{k,k-1} (\tilde{\omega}_{k-1,0}^C \tilde{\omega}_{k-1,0}^C + \tilde{\varepsilon}_{k-1,0}^C) c_{k,k-1}^T + 2\omega_{k,k-1}^C c_{k,k-1} \tilde{\omega}_{k-1,0}^C c_{k,k-1}^T \tilde{u}_3 \\
\vec{\gamma}_{k0}^C &= c_{k,k-1} \vec{\gamma}_{k-1,0}^C + \gamma_{k,k-1}^C + c_{k,k-1} (\tilde{\omega}_{k-1,0}^C \tilde{\omega}_{k-1,0}^C + \tilde{\varepsilon}_{k-1,0}^C) \vec{r}_{k,k-1}^C, \quad \vec{\gamma}_{10}^C = \dot{\lambda}_{10}^C \vec{u}_3.
\end{aligned} \tag{13}$$

The following matrix relations give the *kinematical conditions of connectivity* for the relative velocities:

$$\begin{aligned}
v_{10}^A \vec{u}_i^T \vec{u}_3 + \omega_{21}^A L \vec{u}_i^T a_{20}^T \tilde{u}_3 \vec{u}_1 &= \dot{\vec{r}}_0^P \\
v_{10}^B \vec{u}_i^T \vec{u}_3 + \omega_{21}^B L \vec{u}_i^T b_{20}^T \tilde{u}_3 \vec{u}_1 &= \dot{\vec{r}}_0^P \quad (i = 2, 3) \\
v_{10}^C \vec{u}_j^T \vec{u}_3 - \omega_{21}^C \{ L \vec{u}_j^T c_{20}^T \tilde{u}_3 c_{32}^T \vec{u}_2 - r \vec{u}_j^T c_{20}^T \tilde{u}_3 c_{32}^T \vec{u}_2 \} - \\
&- \omega_{32}^C L \vec{u}_j^T c_{30}^T \tilde{u}_3 \vec{u}_2 + \omega_{54}^C L \vec{u}_j^T c_{50}^T \tilde{u}_3 \vec{u}_1 &= \dot{\vec{r}}_0^P \quad (j = 1, 2, 3) \\
\omega_{54}^C &= \omega_{21}^C + \dot{\theta}.
\end{aligned} \tag{14}$$

The relations (14) give the Jacobian of the mechanism. This matrix is an essential element for the analysis of the robot workspace. Also, these relations offer a matrix closed-form for the velocities $v_{10}^A, v_{10}^B, v_{10}^C, \omega_{21}^A, \omega_{21}^B, \omega_{21}^C, \omega_{32}^C, \omega_{54}^C$ of the parallel manipulator.

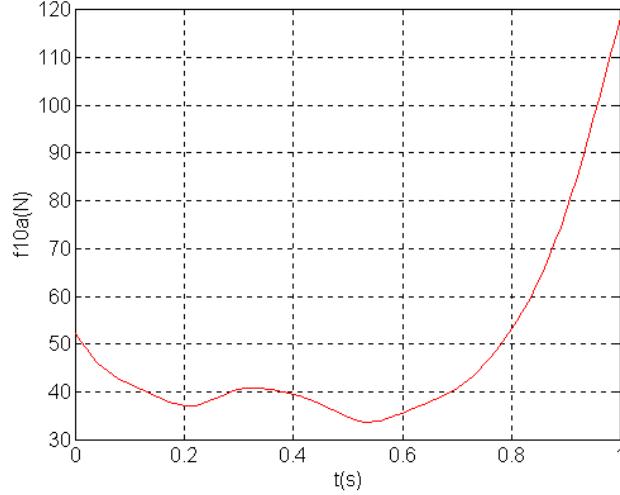


Fig. 3 Force f_{32}^A of first actuator

Let us assume that the manipulator has a virtual motion determined by the velocities $v_{10c}^{Cv} = 1, v_{10c}^{Av} = 0, v_{10c}^{Bv} = 0$. The characteristic virtual velocities, expressed as function of robot's position are given by the connectivity conditions

(14). Some other compatibility relations can be obtained if other two virtual movements are considered: $v_{10a}^{Av} = 1$, $v_{10a}^{Bv} = 0$, $v_{10a}^{Cv} = 0$ and $v_{10b}^{Bv} = 1$, $v_{10b}^{Cv} = 0$, $v_{10b}^{Av} = 0$.

Again, the relative accelerations $\gamma_{10}^A, \gamma_{10}^B, \gamma_{10}^C, \varepsilon_{21}^A, \varepsilon_{21}^B, \varepsilon_{21}^C, \varepsilon_{32}^C, \varepsilon_{54}^C$ of the components of this robot are given by some new conditions of connectivity, which are obtained from the time derivative of (14) relations. The following relations results:

$$\begin{aligned} \gamma_{10}^A \vec{u}_i^T \vec{u}_3 + \varepsilon_{21}^A L \vec{u}_i^T a_{20}^T \vec{u}_3 \vec{u}_1 &= \ddot{r}_0^P - \omega_{21}^A \omega_{21}^A L \vec{u}_i^T a_{20}^T \vec{u}_3 \vec{u}_3 \vec{u}_1 \\ \gamma_{10}^B \vec{u}_i^T \vec{u}_3 + \varepsilon_{21}^B L \vec{u}_i^T b_{20}^T \vec{u}_3 \vec{u}_1 &= \ddot{r}_0^P - \omega_{21}^B \omega_{21}^B L b_{20}^T \vec{u}_3 \vec{u}_3 \vec{u}_1 \quad (i = 2, 3) \\ \gamma_{10}^C \vec{u}_i^T \vec{u}_3 - \varepsilon_{21}^C \{L \vec{u}_j^T c_{20}^T \vec{u}_3 \vec{c}_{32}^T \vec{u}_2 - r \vec{u}_j^T c_{20}^T \vec{u}_3 \vec{c}_{32}^T \vec{u}_2\} - \varepsilon_{32}^C L \vec{u}_j^T c_{30}^T \vec{u}_3 \vec{u}_2 + \\ + \varepsilon_{54}^C L \vec{u}_j^T c_{50}^T \vec{u}_3 \vec{u}_1 &= \ddot{r}_0^P + \omega_{21}^C \omega_{21}^C \{L \vec{u}_j^T c_{20}^T \vec{u}_3 \vec{u}_3 \vec{c}_{32}^T \vec{u}_2 - r \vec{u}_j^T c_{20}^T \vec{u}_3 \vec{u}_3 \vec{c}_{52}^T \vec{u}_1\} + \\ + \omega_{32}^C \omega_{32}^C L \vec{u}_j^T c_{30}^T \vec{u}_3 \vec{u}_2 - \omega_{54}^C \omega_{54}^C r \vec{u}_j^T c_{50}^T \vec{u}_3 \vec{u}_1 + 2 \omega_{21}^C \omega_{32}^C L \vec{u}_j^T c_{20}^T \vec{u}_3 \vec{u}_2 - \\ - 2 \omega_{21}^C \omega_{54}^C r \vec{u}_j^T c_{20}^T \vec{u}_3 \vec{c}_{52}^T \vec{u}_1 \quad (j = 1, 2, 3) \\ \varepsilon_{54}^C &= \varepsilon_{21}^C + \ddot{\theta}. \end{aligned} \quad (15)$$

The relations (14) and (15) represent *the inverse kinematical model* of parallel manipulator.

4. Inverse dynamics model

Although the parallel manipulators with less DOF have been investigated to some extent, works on their dynamics are relatively few. Because of existence of multiple closed-loop chains, dynamic analysis of a parallel manipulator is quite complicated.

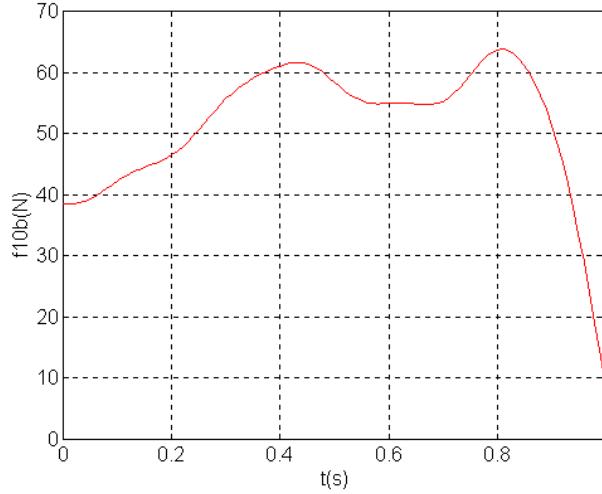
The motion of the movable platform is controlled by three independent pneumatic systems that generate three forces

$$\vec{f}_{32}^A = f_{32}^A \vec{u}_3, \quad \vec{f}_{32}^B = f_{32}^B \vec{u}_3, \quad \vec{f}_{32}^C = f_{32}^C \vec{u}_3, \quad (16)$$

which train the sliders on the guide ways $A_1 z_1^A, B_1 z_1^B, C z_1^C$.

Let us consider that the motion of the platform is known. In these conditions, position, velocity and acceleration of each link and joint are first determined. The force of inertia and the resultant moment of the forces of inertia of the T_k body are determined with respect to A_k joint's centre. On the other hand, the characteristic vectors \vec{f}_k^*, \vec{m}_k^* evaluate the influence of the action of the weight $m_k \vec{g}$ and of other external and internal forces applied to the same element T_k . Then the forces and the moments that are acting each rigid body are definitively determined.

In the inverse dynamic problem, in the present paper, one applies the virtual powers method in order to establish some recursive matrix relations for the forces of the three actuators.

Fig. 4 Force f_{32}^B of second actuator

As the virtual velocities method shows, the dynamic equilibrium condition of the mechanism is that the virtual power of the external, internal and inertia forces, which is developed during a general virtual displacement, must be null. Applying the fundamental equations of the parallel robots dynamics established in compact form by Ştefan Staicu [19], the following matrix relations give the forces exerted on the legs by the sliders along their directions:

$$\begin{aligned}
 f_{10}^A &= \vec{u}_3^T \{ \vec{F}_1^A + \omega_{21a}^{Av} \vec{M}_2^A + \omega_{21a}^{Bv} \vec{M}_2^B + \omega_{21a}^{Cv} \vec{M}_2^C + \\
 &\quad + \omega_{32a}^{Cv} \vec{M}_3^C + \omega_{43a}^{Cv} \vec{M}_4^C + \omega_{54a}^{Cv} \vec{M}_5^C + \omega_{62a}^{Cv} \vec{M}_6^C \} \\
 f_{10}^B &= \vec{u}_3^T \{ \vec{F}_1^B + \omega_{21b}^{Av} \vec{M}_2^A + \omega_{21b}^{Bv} \vec{M}_2^B + \omega_{21b}^{Cv} \vec{M}_2^C + \\
 &\quad + \omega_{32b}^{Cv} \vec{M}_3^C + \omega_{43b}^{Cv} \vec{M}_4^C + \omega_{54b}^{Cv} \vec{M}_5^C + \omega_{62b}^{Cv} \vec{M}_6^C \} \\
 f_{10}^C &= \vec{u}_3^T \{ \vec{F}_1^C + \omega_{21c}^{Av} \vec{M}_2^A + \omega_{21c}^{Bv} \vec{M}_2^B + \omega_{21c}^{Cv} \vec{M}_2^C + \\
 &\quad + \omega_{32c}^{Cv} \vec{M}_3^C + \omega_{43c}^{Cv} \vec{M}_4^C + \omega_{54c}^{Cv} \vec{M}_5^C + \omega_{62c}^{Cv} \vec{M}_6^C \},
 \end{aligned} \tag{17}$$

where one denoted

$$\begin{aligned}
 \vec{F}_k^A &= \vec{F}_{k0}^A + a_{k+1,k}^T \vec{F}_{k+1}^A \\
 \vec{M}_k^A &= \vec{M}_{k0}^A + a_{k+1,k}^T \vec{M}_{k+1}^A + \tilde{r}_{k+1,k}^A a_{k+1,k}^T \vec{F}_{k+1}^A \\
 \vec{F}_{k0}^A &= m_k^A \left[\vec{v}_{k0}^A + (\tilde{\omega}_{k0}^A \tilde{\omega}_{k0}^A + \tilde{\varepsilon}_{k0}^A) \vec{r}_k^{CA} \right] - \vec{f}_k^{*A} \\
 \vec{M}_{k0}^A &= m_k^A \tilde{r}_k^{CA} \vec{v}_{k0}^A + \tilde{J}_k^A \tilde{\varepsilon}_{k0}^A + \tilde{\omega}_{k0}^A \tilde{J}_k^A \tilde{\omega}_{k0}^A - \vec{m}_k^{*A} \\
 \vec{f}_k^{*A} &= -9.806 m_k^A a_{k0} \vec{u}_3 \\
 \vec{m}_k^{*A} &= -9.806 m_k^A \tilde{r}_k^{CA} a_{k0} \vec{u}_3.
 \end{aligned} \tag{18}$$

The relations (17) and (18) represent *the inverse dynamic model* of the 3-DOF spatial parallel manipulator.

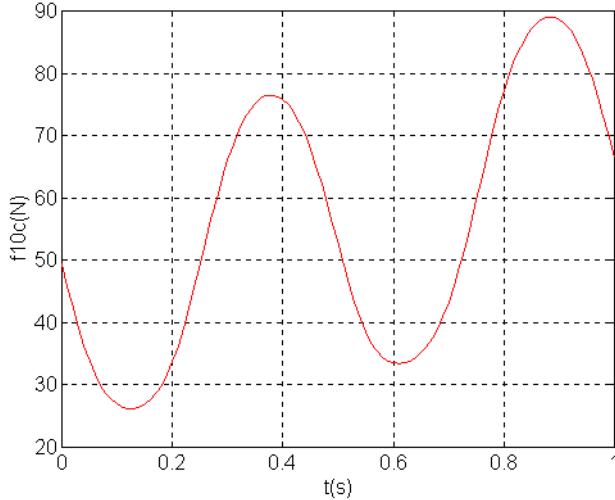


Fig. 5 Force f_{32}^C of third actuator

As applications let us consider a manipulator which has the following characteristics

$$r = 0.1 \text{ m}, R = 0.25 \text{ m}, L = 0.4 \text{ m}$$

$$m_1 = 0.9751 \text{ kg}, m_2 = 0.9803 \text{ kg}, m_3 = 8.1573 \text{ kg}$$

$$\hat{J}_2 = \begin{bmatrix} 0.0006 & & \\ & 0.0524 & \\ & & 0.0524 \end{bmatrix}, \hat{J}_3 = \begin{bmatrix} 0.0269 & & \\ & 0.0658 & \\ & & 0.0501 \end{bmatrix}.$$

Assuming that there is not external force and moment acting on the movable platform, the actuator forces f_{10}^A (Fig. 3), f_{10}^B (Fig. 4), f_{10}^C (Fig. 5) are shown for one second of platform's evolution.

Conclusions

1. Using the Newton-Euler classic method, which takes into account each of rigid bodies separate of the kinematical chains, a system of numerous equations of dynamic equilibrium for all moving body are written and must be solved. The solution of this system leads to all the forces and moments at the joints, including the actuator forces.

2. Analytical calculi involved in the Lagrange formalism are too long and they have risk of making errors. Also, the time for numerical calculus increases with the number of bodies of the device.
3. Within the inverse positional analysis some exact relations giving in real-time the position, velocity and acceleration of each element of a 3-DOF spatial parallel manipulator have been established in closed form in the present study.
4. Based on virtual work principle, the new approach described above is far more efficient and establishes a direct recursive determination of the variation in real-time of the forces of the three actuators. In a context of control, the iterative matrix relations, (17) and (18), given by this simulation dynamic model, can be transformed in a model for automatic command of the spatial manipulator.

R E F E R E N C E S

1. *Clavel, R.*, Delta: a fast robot with parallel geometry, Proceedings of 18th International Symposium on Industrial Robots, Lausanne, 1988.
2. *Cleary, K., Brooks, T.*, Kinematics analysis of a novel 6-DOF parallel manipulator, Proceedings of the IEEE International Conference on Robotics and Automation, 1993.
3. *Coiffet, P.*, La robotique. Principes et applications, Hermès, 1992.
4. *Dasgupta, B., Mruthyunjaya, T.S.*, A Newton-Euler formulation for the inverse dynamics of the Stewart platform manipulator, Mechanism and Machine Theory, 34, 1998.
5. *Denavit, J., Hartenberg, R.*, A kinematic notation for lower-pair mechanisms based on matrices, ASME Journal of Applied Mechanics, 1955.
6. *Geng, Z., Haynes, L.S., Lee, J.D., Carroll, R.L.*, On the dynamic model and kinematic analysis of a class of Stewart platforms, Robotics and Autonomous Systems, 9, 1992.
7. *Hervé, J.-M., Sparacino, F.*, Star. A New Concept in Robotics, Proceedings of the Third International Workshop on Advances in Robot Kinematics, Ferrara, 1992.
8. *Husty, M.L.*, An algorithm for solving the direct kinematics of the Stewart-Gough platforms, Mechanism and Machine Theory, 31, 4, 1996.
9. *Innocenti, C., Parenti-Castelli, V.*, Echelon form solution of direct kinematics for general fully-parallel spherical wrist, Mechanism and Machine Theory, 28, 4, 1993
10. *Li, Y-W., Wang, J., Wang, L-P., Liu, X-J.*, Inverse dynamics and simulation of a 3-DOF spatial parallel manipulator, Proceedings of the IEEE International Conference on Robotics & Automation, Taipei, Taiwan, 2003.
11. *Liu, X-J., Wang, J., Wang, L-P.*, On the analysis of a new spatial three-degrees-of-freedom parallel manipulator, IEEE Transaction on Robotics and Automation, 17, 2001.
12. *Notash, L., Podhorodeski, R.*, Complete forward displacement solution for a class of three-branch parallel chains, International Journal of Robotic Systems, 11, 6, 1994.
13. *Pang, H., Shahingpoor, M.*, Inverse dynamics of a parallel manipulator, Journal of Robotic Systems, 11, 8, 1994.
14. *Parenti-Castelli, V., Di Gregorio, R.*, A new algorithm based on two extra-sensors for real-time computation of the actual configuration of generalized Stewart-Gough manipulator, Journal of Mechanical Design, 122, 2000.
15. *Pierrot, F., Company, O.*, H4: A new family of 4-DOF parallel robots, Proceedings of the IEEE/ASME International Conference on Advanced Intelligent Mechatronics, 1999.

16. *Staicu, Șt.*, Aplicatii ale calculului matriceal in mecanica solidelor, Edit. Académie Roumaine, Bucharest, 1986..
17. *Staicu, Șt.*, Mecanica teoretica, Edit. Didactica & Pedagogica, Bucharest, 1998.
18. *Staicu, Șt.*, Modèle dynamique en robotique, Scientific Bulletin, Series D, Mechanical Engineering, University „Politehnica” of Bucharest, 61, 1999.
- 19.. *Staicu, Șt.*, Méthodes matricielles en dynamique des mécanismes, Scientific Bulletin, Series D, Mechanical Engineering, University „Politehnica” of Bucharest, 62, 3, 2000.
20. *Staicu, Șt.*, *Carp-Ciocardia, D.C.*, On an inverse dynamic problem in robotics, Proceedings of the 12th International DAAAM Symposium, Viena, October 2001.
21. *Staicu, Șt.*, *Carp-Ciocardia, D.C.*, Dynamic analysis of Clavel's Delta parallel robot, Proceedings of the IEEE International Conference on Robotics & Automation ICRA'03, Taipei, Taiwan, 2003.
22. *Stewart, D.*, A Platform with Six Degrees of Freedom, Proc. Inst. Mech. Eng., 1, 15, 1965.
23. *Thusty, J.*, *Ziegert, J.*, *Ridgeway, S.*, Fundamental comparison of the use of serial and parallel kinematics for machine tools, Annals of CIRP, 49, 1999.
24. *Tsai, L-W.*, Robot analysis: the mechanics of serial and parallel manipulators, John Wiley & Sons, Inc., New York, 1999.
25. *Tsai, L-W.*, *Stamper, R.*, A parallel manipulator with only translational degrees of freedom, ASME Design Engineering Technical Conferences, Irvine, CA, 1996.
26. *Wohlhart, K.*, Displacement analysis of the general spherical Stewart platform, Mechanism and Machine Theory, 29, 4, 1994.
27. *Wen, F.*, *Liang, C.*, Displacement analysis of the 6-6 Stewart platform mechanism, Mechanism and Machine Theory, 29, 4, 1994.
28. *Zhang, C-D. Song, S-M.*, An efficient method for inverse dynamics of manipulators based on the virtual work principle, Journal of Robotic Systems, 10, 5, 1993.
29. *Zhang, D. Fengfeng X. Machebske, C.K.*, Kinematic Analysis of a Spatial 3-dof Parallel Manipulator, CCToMM Symposium on Mechanisms, Machines and Mechatronics, Saint-Hubert (Montréal), Juin 2001.
30. *Zsombor-Murray, P.J.*, Kinematics Analysis of Clavel's „Delta” Robot, CCToMM Symposium on Mechanisms, Machines and Mechatronics, Saint-Hubert (Montréal), Juin 2001.
31. *Staicu, Șt.*, *Predoi, M.V.*, Modèle théorique en mécanique des robots, Rev. Roum. Sci. Tech.-Méc. Appl., 45, 4-6, 2000.
32. *Staicu, Șt.*, Planetary Gear Train for Robotics, Proceedings of the IEEE International Conference on Mechatronics ICM/HIMA'05, Taipei, Taiwan; 2005.
33. *Staicu, Șt.*, *Zhang, D.*, *Rugescu, R.*, Dynamic modelling of a 3-DOF parallel manipulator using recursive matrix relations, Robotica, Cambridge University Press, 24, 1, 2006.
34. *Angeles, J.*, Fundamentals of Robotic Mechanical Systems: Theory, Methods and Algorithms, Springer-Verlag, New York, 1997.