

REPURPOSING PHARMACEUTICAL WASTE: EXPIRED MOLDAMIN AS A HIGH-EFFICIENCY, ECO-FRIENDLY CORROSION INHIBITOR FOR STEEL IN ACIDIC MEDIA

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This research evaluates the effectiveness of expired moldamin, a pharmaceutical waste material, as a corrosion inhibitor for AISI 1010 steel exposed to aqueous solutions of 1 M hydrochloric acid (HCl) and 1 M sulfuric acid (H₂SO₄) at 25 ± 2 °C. The study utilized electrochemical impedance spectroscopy (EIS) and potentiodynamic polarization (Tafel analysis) to assess corrosion behavior. Adsorption properties were investigated using the Langmuir adsorption isotherm, and thermodynamic activation parameters were analyzed to determine the spontaneity of the adsorption process. Results indicate that moldamin acts as a mixed-type inhibitor, providing notable protection through both anodic and cathodic mechanisms, with particularly strong performance in sulfuric acid. The highest inhibition efficiencies observed were 89.23% in HCl and 88.7% in H₂SO₄ at a concentration of 10⁻³ M. Surface characterization using 3D laser microscopy confirmed a marked decrease in surface roughness. Overall, the findings highlight moldamin's potential for both corrosion control and sustainable management of pharmaceutical waste.

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1. Introduction

Corrosion is an inevitable degradation process that severely impacts metallic infrastructure in acidic environments. Low-carbon steels like AISI 1010 are prized in automotive, construction, and transportation for their mechanical properties and cost, yet they are highly susceptible to acidic corrosion. This leads to significant economic consequences from material loss, structural weakening, and high maintenance. Developing robust corrosion protection is therefore essential for extending the service life of steel infrastructure [1,2].

There are various techniques to protect metallic materials from corrosion, with the use of corrosion inhibitors being particularly favored due to their efficiency, simplicity of application, and cost-effectiveness [3,4]. Corrosion inhibitors are chemical agents that slow metal deterioration when added in small quantities to corrosive environments. Effective inhibitors are critical for enhancing the longevity of steel infrastructure. However, traditional inhibitors such as chromates and phosphates are toxic and environmentally hazardous, driving the need for safer, eco-friendly alternatives [5,6].

In recent years, attention has shifted increasingly to environmentally friendly and sustainable corrosion inhibitors derived from plant extracts, organic substances, and waste materials. Among these, pharmaceutical compounds (especially expired medications) have gained recognition as unconventional but promising corrosion inhibitors [7]. Although typically considered waste, expired pharmaceuticals contain complex molecular structures rich in heteroatoms such as oxygen, nitrogen, sulfur, and fluorine, as well as π -electrons, which enhance their ability to be adsorbed onto metal surfaces effectively [8,9]. Moldamin, characterized by its sulfur- and nitrogen-containing moieties, demonstrates high affinity for steel surfaces in acidic environments, enabling effective corrosion inhibition through surface complexation and electrochemical interaction [10,11]. Several studies have reported the effectiveness of antibiotics such as amoxicillin, paracetamol, and atorvastatin in mitigating corrosion in various metallic systems, demonstrating their potential as sustainable inhibitors [12–14].

Repurposing expired Moldamin also supports global sustainability by reducing chemical waste and promoting a circular economy. This study therefore not only assesses its corrosion protection but also contributes to waste valorization strategies for industrial use [15].

While pharmaceuticals show promise as corrosion inhibitors, research remains largely exploratory and limited to mild steel in HCl. Performance in other

environments, such as sulfuric acid on specific grades like AISI 1010 steel, is inadequately investigated.

This research therefore systematically assesses Moldamin as a cost-efficient, green inhibitor for AISI 1010 steel in acid. It characterizes its adsorption behavior, quantifies inhibition efficiency, and evaluates adherence to adsorption isotherms to determine its viability as a sustainable alternative.

2. Methodology

2.1. Materials

The corrosion behavior of AISI 1010 steel in hydrochloric acid (HCl, Riedel-de Haën, 37%) and sulfuric acid (H₂SO₄, Merck, p.a., 95-97%) solutions was investigated, along with the inhibitory efficacy of the expired pharmaceutical compound Moldamin (Moldamin, 1,200,000 IU per vial; Antibiotice S.A., Romania). Inhibitor concentrations ranging from 10⁻⁶ to 10⁻³ mol/L were employed. Moldamin (C₄₈H₅₆N₆O₈S₂) IUPAC name is (2S,5R,6R)-3,3-dimethyl-7-oxo-6-[(phenylacetyl)amino]-4-thia-1-azabicyclo [3.2.0] heptane-2-carboxylic acid benzathine (1:1), and the chemical structure is presented in Fig. 1.

The elemental composition was determined using optical emission spectrometry (Thermo Electron Corporation Genesys, Thermo Fisher Scientific, United States), and they are presented in Table 1

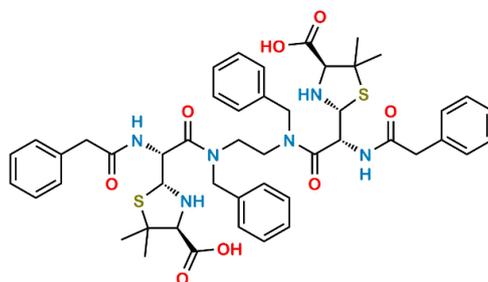


Fig. 1. Moldamin chemical structure

Table 1

Chemical composition of the AISI 1010 steel sample

Element	Fe	Cu	Mn	Si	C	Al	Cr	Mo
Wt%	98.82	0.483	0.372	0.1751	0.0941	0.067	0.06	0.030

2.2. Methods

2.2.1. Specimens' preparation

The preparation of AISI 1010 steel specimens for subsequent testing adhered to ASTM G1. The process commenced with mechanical polishing through a graded series of silicon carbide abrasive papers (120 to 2000 grit). Specimens were then subjected to ultrasonic cleaning in ethanol for contaminant removal,

followed by extensive rinsing in distilled water. After drying, specimens were stored in a desiccator to maintain surface integrity before testing.

2.2.2. Surface roughness

The samples were prepared under five distinct conditions: (1) polished AISI 1010 steel serving as the control, (2) after immersion in 1 M HCl, (3) after immersion in 1 M H₂SO₄, (4) following immersion in 1 M HCl containing 10⁻³ M Moldamin; and (5) following immersion in 1 M H₂SO₄ containing 10⁻³ M Moldamin.

Surface roughness was evaluated using a laser scanning three-dimensional measuring microscope (LEXT OLS 4000, Olympus, Japan). Initial two-dimensional surface images were acquired, followed by three-dimensional surface profiling using a 405 nm laser source.

2.2.3. Electrochemical measurements

The linear polarization (Tafel method) and electrochemical impedance spectroscopy (EIS) [16] were employed to investigate and highlight the corrosion-inhibiting properties of Moldamin on AISI 1010 steel. The experimental setup used a conventional 75 mL glass cell with a four-electrode configuration, connected to an AUTOLAB PGSTAT 302N potentiostat. The system included two graphite counter electrodes, an AISI 1010 steel working electrode, and a saturated Ag/AgCl reference electrode (Fig. 2), ensuring stable current distribution and measurement accuracy. Before each experiment, the working electrode surface was polished to achieve a uniform surface using different sandpapers of varying grit sizes to achieve a smooth finish, then thoroughly cleaned to remove any residual particles or contaminants and rinsed with distilled water to remove impurities, ensuring it was suitable for accurate electrochemical testing and corrosion studies.

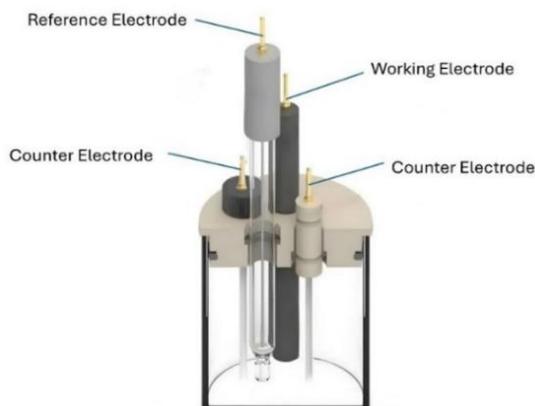


Fig. 2. Schematic diagram of cell configuration

Following this preparation, the electrode's potential stabilized for 45 minutes to ensure equilibrium and reliable measurement conditions. Linear polarization tests were performed at 1 mV/s (± 250 mV vs. OCP) under quasi-stationary conditions at 25 °C. Measurements included uninhibited solution and Moldamin concentrations from 10^{-6} to 10^{-3} M, with triplicate trials/concentration. Tafel curves were then extrapolated to estimate the values of polarization parameters such as corrosion potential (E_{corr}), corrosion current density (i_{corr}), and corrosion rate (CR). From such parameters, the inhibition efficiency (IE) could also be estimated from Eq. 1 [16] as follows.

$$IE(\%) = \frac{i_{corr}^o - i_{corr}^{inh}}{i_{corr}^o} * 100 \quad (1)$$

Where: i_{corr}^o is the current density in the absence of Moldamin [$\mu\text{A}/\text{cm}^2$]; i_{corr}^{inh} is the current density in the presence of Moldamin [$\mu\text{A}/\text{cm}^2$].

EIS measurements were conducted using a Metrohm Autolab PGSTAT 302N potentiostat at the open circuit potential (OCP). Spectra were acquired over a frequency range of 0.01 Hz to 100 kHz with a 10 mV AC perturbation. Data from three repeated tests ($n=3$) were modeled in Nova 2.1.7 software using the equivalent circuit shown in Fig. 3, which consists of solution resistance (R_s) in series with a parallel constant phase element (CPE) and polarization resistance (R_p). The composite R_p encompasses the contributions of charge transfer resistance (R_{ct}), double-layer dispersion resistance (R_d), inhibitor-derived surface film resistance (R_f), and adsorption-mediated accumulation resistance (R_a) [17–19].

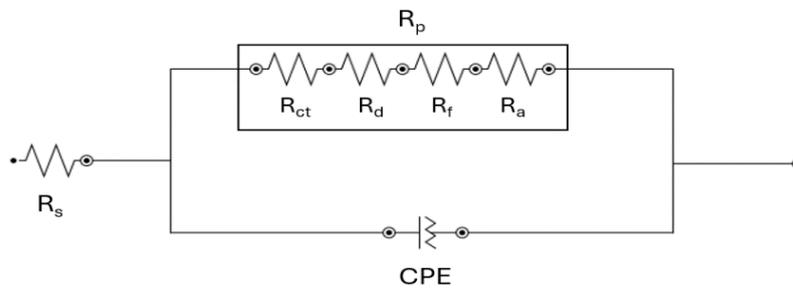


Fig. 3. Equivalent circuit used for simulation of data

To model the capacitance associated with depressed Nyquist semicircles, a constant-phase element (CPE), representing a non-ideal capacitor, replaces the pure capacitor in the circuit model. Its impedance is defined by [20]

$$Z_{CPE} = \frac{1}{Y_o(j\omega)^n} \quad (2)$$

Where: Z_{CPE} : the impedance of CPE; Y_o : the CPE coefficient (representing admittance, the reciprocal of impedance); ω : the angular frequency given by $\omega=2*\pi*f$ (having units in rad/s); n : A dimensionless parameter ($0 \leq n \leq 1$) that describes the degree of non-ideality:

The double-layer capacitance (C_{dl}) can be evaluated as follows

$$C_{dl} = \frac{Y_o \omega^{n-1}}{\sin(n(\frac{\pi}{2}))} \quad (3)$$

Where: ω is given by:

$$\omega_{\max} = 2 * \pi * f_{\max} \quad (4)$$

corresponding to the peak frequency of the negative imaginary impedance component ($-Z_{\text{imag}}$).

Then, the inhibition efficiency can be calculated from another perspective using polarization resistance (R_p) as follows [16].

$$IE(\%) = \frac{R_p^{inh} - R_p^0}{R_p^{inh}} * 100 \quad (5)$$

Where: R_p^{inh} is the polarization resistance in the presence of Moldamin [Ω]; R_p^0 is the polarization resistance in the absence of Moldamin [Ω].

2.2.4. Adsorption isotherms

Adsorption isotherms provide fundamental insights into how inhibitors interact with the AISI 1010 steel surface, explaining the corrosion inhibition mechanism. This adsorption process depends critically on the inhibitor's molecular structure, its charge distribution, and the nature of the charged metal surface and acidic media [17].

The surface coverage calculated using Eq. 6

$$\theta = \frac{CR^o - CR^{inh}}{CR^o} \quad (6)$$

Where: CR^o : the corrosion rate of steel in the absence of Moldamin [mm/year]; CR^{inh} : the corrosion rate of steel in the presence of Moldamin [mm/year].

The Langmuir adsorption isotherm is applied as in Eq.7 [17]

$$\frac{C_{inh}}{\theta} = C_{inh} + \frac{1}{k_{ads}} \quad (7)$$

Where: C_{inh} is the concentration of the inhibitor; θ is the surface coverage calculated from Eq. 6; K_{ads} is the adsorption constant, obtained from the intercept of the straight line, relates to the standard free energy of adsorption in Eq. 8 [21].

$$\Delta G_{ads}^0 = -RT \ln(55.5 K_{ads}) \quad (8)$$

Where: R: is the universal gas constant [J/M. K]; T : is the absolute temperature[K].

3. Results and discussion

3.1. Linear polarization

Tafel curves shown in Fig. 4 and polarization parameters for AISI 1010 steel corrosion in both acid media, 1 M HCl and 1 M H₂SO₄, i.e., corrosion potential (E_{corr}), corrosion current density (i_{corr}), and corrosion rate (CR) were determined by

extrapolating the Tafel curves. Inhibition efficiency (IE%, Eq. 1) was calculated; results are presented in Table 2.

Tafel polarization confirms the high inhibition efficiency of Moldamin for AISI 1010 steel in 1 M HCl and H₂SO₄, which increases with concentration up to a maximum at 10⁻³ M. This concentration-dependent behavior indicates greater surface coverage by Moldamin molecules, approaching monolayer adsorption at optimal concentration.

Notably, the Tafel curves show a parallel shift of both anodic and cathodic branches, indicating that Moldamin acts as a mixed-type inhibitor. This implies that it concurrently suppresses the anodic dissolution of iron ($\text{Fe} \rightarrow \text{Fe}^{2+} + 2\text{e}^-$) and the cathodic hydrogen evolution reaction ($2\text{H}^+ + 2\text{e}^- \rightarrow \text{H}_2$). Such dual inhibition points to effective surface interaction with active corrosion sites.

Moldamin's similar inhibition in both HCl and H₂SO₄ underscores its versatility, indicating an anion-independent mechanism. This likely results from strong adsorption via both chemisorption—through donor-acceptor interactions—and physisorption. These findings confirm its strong potential as a robust, broad-spectrum acidic corrosion inhibitor.

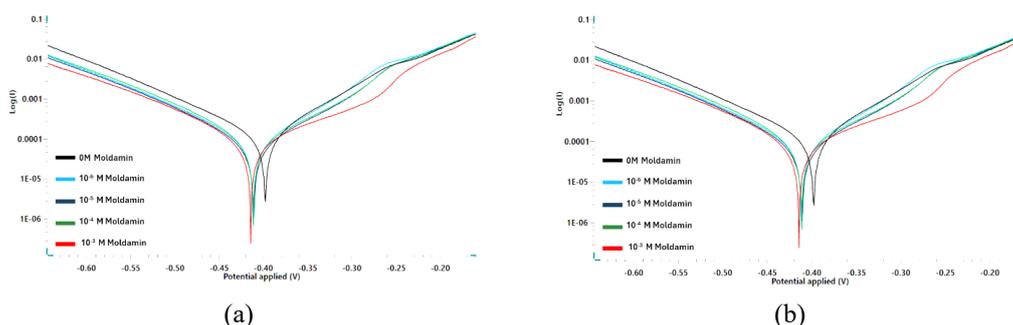


Fig. 4 Tafel curves on AISI 1010 steel electrode in (a) 1 M HCl and (b) 1 M H₂SO₄ in the absence/presence of the moldamin.

As shown in Table 2, Tafel polarization data confirms Moldamin's concentration-dependent inhibition on AISI 1010 steel. In 1M HCl, i_{CORR} decreased from 142.06 to 15.30 $\mu\text{A}/\text{cm}^2$ (89.23% efficiency), while in 1M H₂SO₄, it dropped from 361.76 to 43.42 $\mu\text{A}/\text{cm}^2$ (88.70% efficiency) at the optimal 10⁻³ M concentration.

The minimal E_{CORR} shifts (less than 30 mV) in both media confirm Moldamin acts as a mixed-type inhibitor [22], affecting both anodic and cathodic reactions. The moderate cathodic shifts (from -397.91 to -414.36 mV in HCl and from -387.87 to -395.51 mV in H₂SO₄) suggest a slightly greater influence on the cathodic process.

The corrosion penetration rate (CR) underscores Moldamin's practical efficacy. In 1M HCl, v_{CORR} was reduced from 1.6507 to 0.17772 mm/year (89.2%

reduction). Even in the more aggressive H_2SO_4 , it was lowered from 4.2048 to 0.5046 mm/year. These final rates are well below typical industrial thresholds, confirming its practical applicability in both environments.

Despite H_2SO_4 being a more aggressive environment than HCl, Moldamin achieves remarkably consistent and high inhibition efficiencies (~89% in HCl and ~89% in H_2SO_4). This anion-independent performance demonstrates a robust inhibition mechanism, making it a versatile and promising candidate for various acidic industrial applications.

Table 2

Polarization parameters for an AISI 1010 steel rod's corrosion process in an acid solution in the presence and absence of Moldamin.

Media	Moldamin Conc. (M)	E_{corr} (mV)	i_{corr} ($\mu\text{A}/\text{cm}^2$)	CR (mm/year)	IE %	θ
HCL	0	-397.91	142.06	1.6507	0.00	0
	10^{-6}	-411.66	50.99	0.59255	64.10	0.641
	10^{-5}	-410.92	37.53	0.43613	73.58	0.7358
	10^{-4}	-411.38	20.11	0.23369	85.84	0.8584
	10^{-3}	-414.36	15.30	0.17772	89.23	0.8923
H_2SO_4	0	-387.87	361.76	4.2048	0.00	0
	10^{-6}	-408.72	154.03	1.7898	57.43	0.5743
	10^{-5}	-391.54	128.23	1.4911	66.60	0.666
	10^{-4}	-390.38	74.66	0.8675	80.57	0.8057
	10^{-3}	-395.51	43.42	0.5046	88.70	0.887

3.2. Electrochemical impedance spectroscopy

Nyquist plots (Fig. 5) show the EIS behavior of AISI 1010 steel in 1 M HCl and H_2SO_4 with and without Moldamin. All spectra display a single, depressed capacitive loop, indicative of a charge transfer-controlled process. The diameter of this semicircle, corresponding to the charge transfer resistance (R_{ct}), increased markedly with inhibitor concentration in both acids.

This systematic increase in R_{ct} , reaching a maximum at 10^{-3} M, demonstrates a concentration-dependent inhibition effect. The trend confirms that Moldamin adsorbs onto the steel surface, forming a protective film that impedes charge transfer. Although R_{ct} values were slightly lower in H_2SO_4 , the inhibitor's strong performance in both media suggests effective adsorption via donor-acceptor interactions between its heteroatoms (N, O) and the iron surface. The non-ideal semicircles are attributed to surface heterogeneities common in inhibitor studies [23].

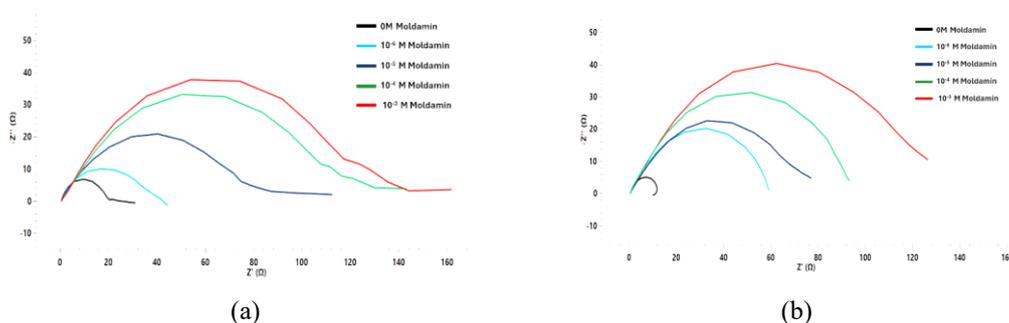


Fig. 5. Nyquist plot for AISI 1010 steel electrode in (a) 1 M HCL, (b) 1 M H₂SO₄ in the absence/presence of Moldamin

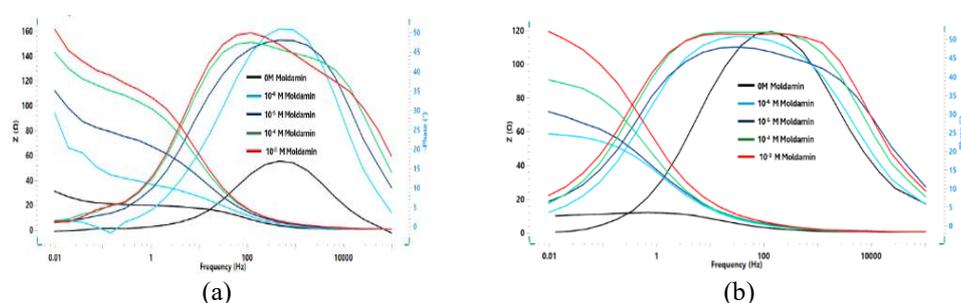


Fig. 6. Bode plot for AISI 1010 steel electrode in (a) 1 M HCL, (b) 1 M H₂SO₄ in the absence/presence of Moldamin

Bode plots (Fig. 6) show the frequency response of AISI 1010 steel in uninhibited and Moldamin-inhibited 1 M HCl and H₂SO₄. In both acids, $|Z|$ values increased significantly at low frequencies (0.01–1 Hz) with inhibitor concentration, reaching a maximum at 10^{-3} M, indicating enhanced barrier resistance from adsorbed Moldamin.

Phase angle curves broadened and shifted toward more negative values with concentration, reflecting formation of a more capacitive, protective surface film. Although absolute impedance was lower in H₂SO₄, the consistent trends—including intensified phase angle peaks approaching 50° and near-linear $|Z|$ slopes—confirm effective inhibitor adsorption and transition toward diffusion-controlled behavior in both media [24].

Table 3

Electrochemical impedance parameters for an AISI 1010 steel rod's corrosion process in an acid solution in the presence and absence of Moldamin.

Media	Moldamin Conc. (M)	R_s (Ω)	C_{dl} ($\mu\text{F cm}^{-2}$)	R_p (Ωcm^2)	IE %
	0	0.5903	113.956	20.963	0.00
	10^{-6}	0.6664	88.778	37.965	44.78

HCL	10^{-5}	0.8954	73.341	77.64	73.00
	10^{-4}	1.4068	55.055	112.16	81.31
	10^{-3}	1.6392	40.155	123.44	83.02
H ₂ SO ₄	0	0.87518	128.875	22.496	0.00
	10^{-6}	1.3749	87.417	59.331	62.08
	10^{-5}	1.5429	71.858	71.551	68.56
	10^{-4}	1.4113	50.858	94.259	76.13
	10^{-3}	1.5953	37.375	126.44	82.21

The electrochemical impedance spectroscopy (EIS) results presented in Table 3 reveal significant changes in the impedance parameters of AISI 1010 steel in both 1 M HCl and 1 M H₂SO₄ media upon the addition of varying concentrations of Moldamin. In both acidic environments, a marked increase in polarization resistance (R_p) was observed with increasing inhibitor concentration, indicating a strong corrosion-inhibiting effect. Specifically, R_p increased from 20.96 $\Omega \cdot \text{cm}^2$ (blank solution) to 123.44 $\Omega \cdot \text{cm}^2$ in 1 M HCl, and from 22.50 $\Omega \cdot \text{cm}^2$ to 126.44 $\Omega \cdot \text{cm}^2$ in 1 M H₂SO₄, upon the addition of 10^{-3} M Moldamin. This trend suggests that Moldamin forms a protective film on the steel surface, effectively impeding the charge transfer process responsible for corrosion.

Concomitantly, the double-layer capacitance (C_{dl}) showed a substantial decrease as the inhibitor concentration increased. In the case of 1 M HCl, C_{dl} dropped from 113.96 $\mu\text{F} \cdot \text{cm}^{-2}$ to 40.15 $\mu\text{F} \cdot \text{cm}^{-2}$, while in 1 M H₂SO₄, it decreased from 128.88 $\mu\text{F} \cdot \text{cm}^{-2}$ to 37.38 $\mu\text{F} \cdot \text{cm}^{-2}$. The reduction in C_{dl} is indicative of the adsorption of Moldamin molecules onto the steel surface, displacing water molecules and reducing the local dielectric constant. This behavior points to the formation of a more compact and less permeable inhibitor layer, which effectively suppresses the corrosion reaction.

Furthermore, the inhibition efficiency (IE%) progressively improved with higher Moldamin concentrations, reaching 83.02% in 1 M HCl and 82.21% in 1 M H₂SO₄ at 10^{-3} M. These results confirm that Moldamin acts as a highly effective corrosion inhibitor in both media, likely through a mixed-type inhibition mechanism involving adsorption on both anodic and cathodic sites. Overall, the EIS data support the conclusion that Moldamin offers substantial protective performance against acid-induced corrosion of AISI 1010 steel, with optimal inhibition efficiency achieved at the highest tested concentration[25]. The overall trends observed in both the impedance modulus and phase angle plots are consistent with the characteristic response of mixed-type corrosion inhibitors such as Moldamin, which simultaneously suppress anodic metal dissolution and cathodic hydrogen evolution. This dual inhibition behavior reinforces the notion that Moldamin not only mitigates the rate of corrosion but also modifies the

electrochemical interface of the steel surface, leading to conditions that are less favorable for corrosion processes to occur.

3.3. Adsorption Isotherm

Fig. 7 shows a linear relationship between $\frac{C_{inh}}{\theta}$ and C_{inh} with a slope near unity, indicating that the inhibitor follows the Langmuir adsorption model described by Eq. 7.

The literature reports that ΔG_{ads}^0 values of approximately -20 kJ/mol are characteristic of physical adsorption, whereas values near -40 kJ/mol imply chemical adsorption[26]. The adsorption behavior of Moldamin on AISI 1010 steel in 1 M HCl and 1 M H₂SO₄ media was evaluated using the Langmuir isotherm model. Excellent linear fits ($R^2 = 0.99981$ in HCl and 0.9999 in H₂SO₄ in C_{inh}/θ versus C_{inh} plots validate Langmuir adsorption. The behavior implies monolayer inhibitor coverage with homogeneous adsorption sites. The calculated adsorption equilibrium constants K_{ads} were $4.13 \times 10^5 \text{ M}^{-1}$ in HCl and $1.93 \times 10^5 \text{ M}^{-1}$ in H₂SO₄, indicating stronger adsorption in the hydrochloric medium. Standard free energy of adsorption ΔG_{ads}^0 was calculated according to Eq. 8 yielding values of -44.5 kJ/mol for HCl and -40.1 kJ/mol for H₂SO₄. These negative and large values (more negative than -40 kJ/mol) suggest that the adsorption process is spontaneous and predominantly chemical in nature (chemisorption). The stronger interaction in HCl may be attributed to enhanced electrostatic attraction between the protonated inhibitor species and the negatively charged steel surface in chloride-containing media.

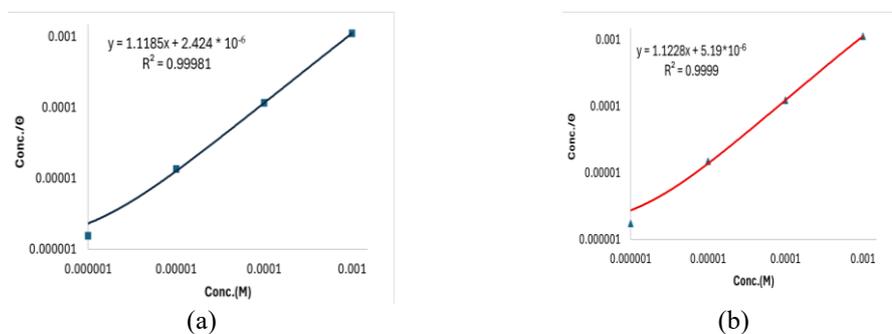


Fig. 7. Langmuir adsorption isotherm plots for AISI 1010 steel at different concentrations of Moldamin in (a) 1 M HCl, and (b) 1 M H₂SO₄ media

3.4. Surface Characterization

The roughness, height, and valley values for all the samples were calculated from the images obtained shown in Fig. 8. Table 4 presents the surface roughness parameters: average roughness (Sa), root mean square roughness (Sq),

maximum peak height (S_p), maximum valley depth (S_v), and maximum height (S_z).

Table 4 presents the calculated surface roughness parameters for AISI 1010 steel samples subjected to different corrosive environments with and without Moldamin. Sample (a), representing the uncorroded or reference surface, exhibits the lowest values across all parameters, with S_a of $0.278 \mu\text{m}$ and S_z of $24.036 \mu\text{m}$, indicating a relatively smooth and unperturbed surface.

In the case of Sample (b), which corresponds to steel exposed to 1 M HCl without any inhibitor, all roughness metrics increased significantly. The values of S_a ($0.427 \mu\text{m}$), S_p ($45.441 \mu\text{m}$), and S_z ($74.744 \mu\text{m}$) point to severe surface degradation, consistent with aggressive corrosion activity induced by hydrochloric acid. This surface damage is further supported by the high S_v value ($32.155 \mu\text{m}$), suggesting pronounced pitting or valley formation due to localized corrosion.

Upon the addition of 10^{-3} M Moldamin in HCl (Sample c), the roughness parameters notably decreased compared to the uninhibited HCl sample. For instance, S_a reduces to $0.418 \mu\text{m}$ and S_z to $47.539 \mu\text{m}$, reflecting the protective influence of Moldamin. The lower S_p and S_v values ($30.875 \mu\text{m}$ and $10.657 \mu\text{m}$, respectively) confirm that the inhibitor effectively mitigates both peak growth and valley formation, likely through adsorption and barrier film formation on the steel surface.

A similar trend is observed in sulfuric acid media. Sample (d), exposed to 1 M H_2SO_4 alone, exhibits significant roughening with S_a of $0.476 \mu\text{m}$ and a maximum S_z of $72.176 \mu\text{m}$, indicating strong corrosive attack. However, the introduction of 10^{-3} M Moldamin in this medium (Sample e) results in substantial surface smoothing. While S_a increases slightly to $0.548 \mu\text{m}$ due to residual roughness, the reduction in S_p and S_v ($33.466 \mu\text{m}$ and $20.112 \mu\text{m}$, respectively) compared to Sample (d) demonstrates Moldamin's inhibitory action in sulfuric acid, reducing both metal dissolution and surface deterioration.

Table 4

Electrochemical impedance parameters for AISI 1010 steel corrosion process in acid solution in the presence and absence of Moldamin.

Sample	S_a [μm]	S_q [μm]	S_p [μm]	S_v [μm]	S_z [μm]
(a)	0.277667	0.388333	19.00733	5.028667	24.036
(b)	0.427	0.579	45.441	32.155	74.744
(c)	0.418	0.531	30.875	10.65633	47.53933
(d)	0.476	0.672	41.689	35.447	72.176
(e)	0.548	0.684	33.466	20.112	53.578

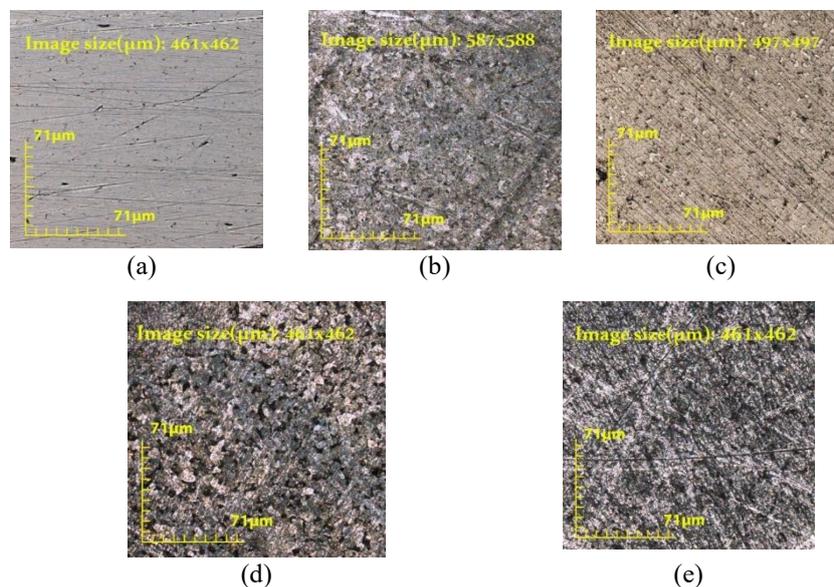


Fig. 8. 3-D laser microscopy surface analysis of AISI 1010 steel of (a) polished AISI 1010 steel, (b) post-immersion in 1M HCl, (c) 1M HCl + 10^{-3} M, (d) post-immersion in 1M H₂SO₄, and (e) 1M H₂SO₄ + 10^{-3} M Moldamin.

Overall, the surface roughness analysis supports the electrochemical data, confirming that Moldamin significantly reduces corrosion-induced topographical damage in both acidic environments, validating its role as an effective mixed-type inhibitor.

4. Conclusion

This study demonstrates that expired Moldamin is an effective and eco-friendly corrosion inhibitor for AISI 1010 steel in acidic media (1 M HCl and 1 M H₂SO₄). At 10^{-3} M concentration, the inhibitor achieved high efficiencies of 89.23% in HCl and 88.70% in H₂SO₄, as determined by both Tafel polarization and electrochemical impedance spectroscopy (EIS). The inhibitor exhibited a mixed-type mechanism, as indicated by parallel shifts in both anodic and cathodic Tafel branches, suppressing both iron dissolution ($\text{Fe} \rightarrow \text{Fe}^{2+} + 2\text{e}^-$) and hydrogen evolution ($2\text{H}^+ + 2\text{e}^- \rightarrow \text{H}_2$).

Adsorption of Moldamin onto the steel surface followed the Langmuir isotherm ($R^2 > 0.9998$), suggesting monolayer formation on a uniform surface. Thermodynamic parameters revealed spontaneous and predominantly chemical adsorption, with highly negative ΔG_{ads}^0 values (-44.5 kJ/mol in HCl and -40.1 kJ/mol in H₂SO₄) and high adsorption equilibrium constants ($K_{ads} = 4.13 \times 10^5 \text{ M}^{-1}$).

in HCl, $1.93 \times 10^5 \text{ M}^{-1}$ in H_2SO_4). These results point to strong donor-acceptor interactions between the inhibitor's heteroatoms (N, O, S) and the metal surface.

EIS measurements confirmed the formation of a protective barrier film, as evidenced by increased polarization resistance (R_p) and decreased double-layer capacitance (C_{dl}) with increasing inhibitor concentration. Surface roughness analysis using 3D laser microscopy further supported the electrochemical findings, showing reduced Sa and Sz parameters in inhibited samples compared to severely corroded controls.

Collectively, these findings establish expired Moldamin as a promising green corrosion inhibitor. Beyond its high efficacy, the repurposing of pharmaceutical waste aligns with circular economy principles, offering an environmentally sustainable approach to corrosion mitigation. Future research should address long-term durability, potential synergistic blends, and real-world application under industrial conditions.

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